The *Journal of Cotton Science 18:207–215 (2014)*
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ENGINEERING AND GINNING

Third Stage Seed-Cotton Cleaning System PM_{10} Emission Factors and Rates for Cotton Gins: Method 201A PM_{10} Sizing Cyclones

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ABSTRACT

This report is part of a project to characterize cotton gin emissions from the standpoint of stack sampling. The impetus behind this project was the urgent need to collect additional cotton gin emissions data to address current regulatory issues. A key component of this study was focused on EPA emission factors for particulate matter with a particle diameter nominally less than or equal to 10 µm (PM_{10}). The 1996 EPA AP-42 emission factors were assigned quality ratings, from A (Excellent) to E (Poor), to assess the quality of the data being referenced. Emission factor quality ratings for cotton gins were extremely low. Cotton gin data received these low ratings because they were collected almost exclusively from a single geographical region. The objective of this study was to collect additional PM_{10} emission factor data for 3rd stage seed-cotton cleaning systems at cotton gins located in regions across the cotton belt based on EPA-approved stack sampling methodology, Method 201A. The project plan included sampling seven cotton gins across the cotton belt. Key factors for selecting specific cotton gins included: 1) facility location, 2) production capacity, 3) processing systems and 4) abatement technologies. Two of the seven gins were equipped with 3rd stage seed-cotton cleaning systems. In terms of capacity, the two gins were typical of the industry, averaging 22.0 bales/h during testing. The 3rd stage seed-cotton cleaning system average emission factors for PM_{10} and total particulate were 0.019 kg/227-kg bale (0.042 lb/500-lb bale) and 0.024 kg/bale (0.054 lb/bale), respectively. The system average PM_{10} emission factor was higher and the system average total particulate emission factor was lower than those currently published in EPA AP-42. Third stage seed-cotton cleaning system PM_{10} emission rate test averages ranged from 0.28 to 0.56 kg/h (0.61-1.24 lb/h). The ratio of 3rd stage seed-cotton cleaning system PM_{10} to total particulate was 79.1%.

U.S. Environmental Protection Agency (EPA) emission factors published in EPA's Compilation of Air Pollution Emission Factors, AP-42 (EPA, 1996b) were assigned a rating that is used to assess the quality of the data being referenced. Ratings can range from A (Excellent) to E (Poor). Current EPA emission factor quality ratings for particulate matter with a particle diameter less than or equal to a nominal 10-µm (PM_{10}) aerodynamic equivalent diameter from cotton gins are extremely low. Cotton gin data received these low ratings because they were collected almost exclusively from a single geographical region (EPA, 1996a). Cotton ginners' associations across the cotton belt, including the National, Texas, Southern, Southeastern, and California associations, agreed that there was an urgent need to collect additional cotton gin emissions data to address current regulatory issues. Working with cotton ginning associations across the country and state and federal regulatory agencies, Oklahoma State University and USDA-Agricultural Research Service (ARS) researchers developed a proposal and sampling plan that was initiated in 2008 to address this need for additional data. This report is part of a series that details cotton gin emissions measured by stack sampling. Each manuscript in the series addresses a specific cotton ginning system. The systems covered in the series include: unloading, 1st stage seed-cotton cleaning, 2nd stage seed-cotton cleaning, 3rd stage seed-cotton cleaning, overflow, 1st stage lint cleaning, 2nd stage lint cleaning, combined lint cleaning, cyclone robber, 1st stage mote, 2nd stage mote, combined mote, mote cyclone robber, mote cleaner, mote trash, battery condenser and master trash. This report focuses on PM_{10} emissions from 3rd stage seed-cotton cleaning systems.

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The 1996 EPA AP-42 average PM_{10} emission factor for the No. 3 dryer and cleaner, which is an equivalent system to the 3rd stage seed-cotton cleaning system, was 0.015 kg (0.033 lb) per 217-kg (480-lb) equivalent bale with a range of 0.014 to 0.016 kg (0.030-0.035 lb) per bale (EPA, 1996a, 1996b). This average and range was based on two tests conducted in one geographical location and the EPA emission factor quality rating was D, which is the second lowest possible rating (EPA, 1996a). The AP-42 average total particulate emission factor for the No. 3 dryer and cleaner was 0.043 kg (0.095 lb) per bale with a range of 0.041 to 0.045 kg (0.091-0.099 lb) per bale. This average and range was based on two tests conducted in one geographical location. The EPA emission factor quality rating was also D.

Seed cotton is a perishable commodity that has no real value until the fiber and seed are separated (Wakelyn et al., 2005). Cotton must be processed or ginned at the cotton gin to separate the fiber and seed, producing 227-kg (500-lb) bales of marketable cotton fiber. Cotton ginning is considered an agricultural process and an extension of the harvest by several federal and state agencies (Wakelyn et al., 2005). Although the main function of the cotton gin is to remove the lint fiber from the seed, many other processes also occur during ginning, such as cleaning, drying, and packaging the lint. Pneumatic conveying systems are the primary method of material handling in the cotton gin. As material reaches a processing point, the conveying air is separated and emitted outside the gin through a pollution control device. The amount of dust emitted by a system varies with the process and the condition of the material in the process.

Cotton ginning is a seasonal industry with the ginning season lasting from 75 to 120 days, depending on the size and condition of the crop. Although the trend for U.S. cotton production remained generally flat at about 17 million bales per year during the last 20 years, production from one year to the next often varied greatly for various reasons, including climate and market pressure (Fig. 1). The number of active gins in the U.S. has not remained constant, steadily declining to fewer than 700 in 2011. Consequently, the average volume of cotton handled by each gin has risen and gin capacity has increased to an average of about 25 bales per hour across the U.S. cotton belt (Valco et al., 2003, 2006, 2009, 2012).

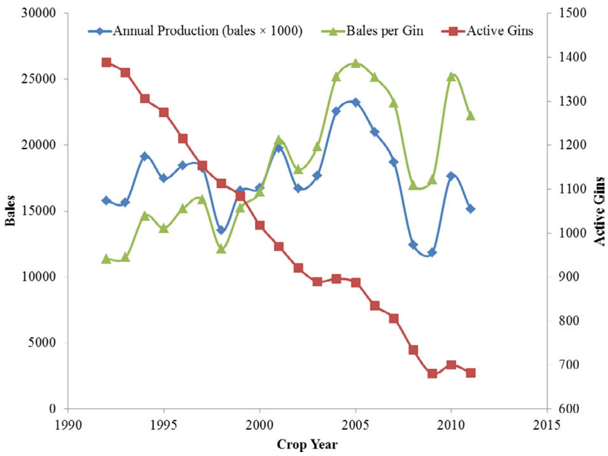

Figure 1. Annual U.S. cotton production, active U.S. gins, and average ginning volume (bales per gin) (NASS, 1993-2012).

Typical cotton gin processing systems include: unloading system, dryers, seed-cotton cleaners, gin stands, overflow collector, lint cleaners, battery condenser, bale packaging system, and trash handling systems (Fig. 2); however, the number and type of machines and processes can vary. Each of these systems serves a unique function with the ultimate goal of ginning the cotton to produce a marketable product. Raw seed cotton harvested from the field is compacted into large units called "modules" for delivery to the gin. The unloading system removes seed cotton either mechanically or pneumatically from the module feed system and conveys the seed cotton to the seed-cotton cleaning systems. Seed-cotton cleaning systems assist with drying the seed cotton and remove foreign matter prior to ginning. Ginning systems also remove foreign matter and separate the cotton fiber from seed. Lint cleaning systems further clean the cotton lint after ginning. The battery condenser and packaging systems combine lint from the lint cleaning systems and compress the lint into dense bales for efficient transport. Cotton gin systems produce some type of by-products or trash, such as rocks, soil, sticks, hulls, leaf material, and short or tangled immature fiber (motes), as a result of processing the seed cotton or lint. These streams of by-products must be removed from the machinery and handled by trash collection systems. These trash systems typically further process the by-products (e.g., mote cleaners) and/or consolidate the trash from the gin systems into a hopper or pile for subsequent removal.

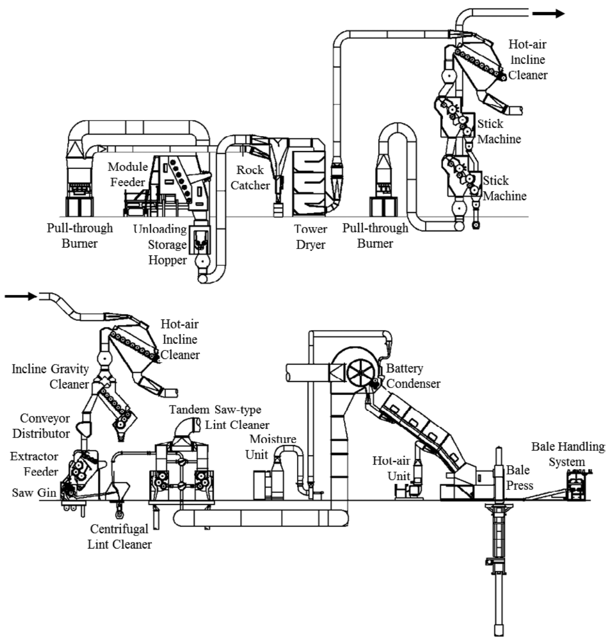

Figure 2. Typical modern cotton gin layout (Courtesy Lummus Corporation, Savannah, GA).

The seed cotton is cleaned and dried in the seed-cotton cleaning systems. In the typical 3rd stage seed-cotton cleaning system (Fig. 3), seed cotton drops from the 2nd stage seed-cotton cleaning system machinery into the hot air pneumatic conveying system of the 3rd stage seed-cotton cleaning system via a rotary airlock and blowbox. The seed cotton is pulled directly into the seed-cotton cleaning machinery and separated from the conveying airstream by the cleaning mechanism (called a “hot-air” cleaner) or separated from the conveying air via a screened separator and dropped into the cleaning machinery. Seed-cotton cleaning machinery includes cleaners or extractors. This system removes foreign matter that includes rocks, soil, sticks, hulls, and leaf material. The airstream from the 3rd stage seed-cotton cleaning system continues through a centrifugal fan to an abatement system; generally one or more cyclones. This cleaning system may use air heated up to 117ºC (350ºF) at the seed cotton and air mixing point to accomplish drying during transport (ASABE, 2007). Based on system configuration, the airstream temperature at the abatement device could range from ambient to about 50% of the mixing-point temperature. The material handled by the abatement system is typically the same as that removed by the seed-cotton cleaning machinery (rocks, soil, sticks, hulls, and leaf material) and lint extracted with the trash (Fig. 4).

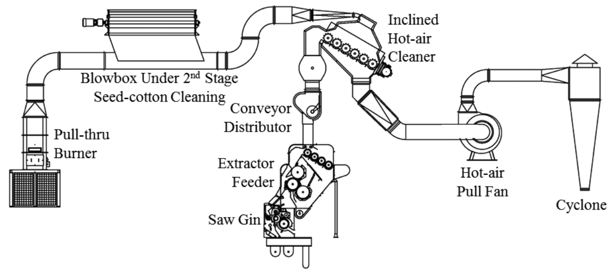

Figure 3. Typical cotton gin 3rd stage seed-cotton cleaning system layout (Courtesy Lummus Corporation, Savannah, GA).

Figure 4. Photograph of typical trash captured by the 3rd stage seed-cotton cleaning system cyclones.

Cyclones are the most common particulate matter abatement devices used at cotton gins. Standard cyclone designs used at cotton ginning facilities are the 2D2D and 1D3D (Whitelock et al., 2009). The first D in the designation indicates the length of the cyclone barrel relative to the cyclone barrel diameter and the second D indicates the length of the cyclone cone relative to the cyclone barrel diameter. A standard 2D2D cyclone (Fig. 5) has an inlet height of D/2 and width of D/4 and design inlet velocity of 15.2 ± 2 m/s (3000 ± 400 fpm). The standard 1D3D cyclone (Fig. 5) has the same inlet dimensions as the 2D2D or may have the original 1D3D inlet with height of D and width D/8. Also, it has a design inlet velocity of 16.3 ± 2 m/s (3200 ± 400 fpm).

The objective of this study was to collect additional PM_{10} emission factor data for 3rd stage seed-cotton cleaning systems with cyclones for emissions control at cotton gins located in regions across the cotton belt based on EPA-approved stack sampling methodologies.

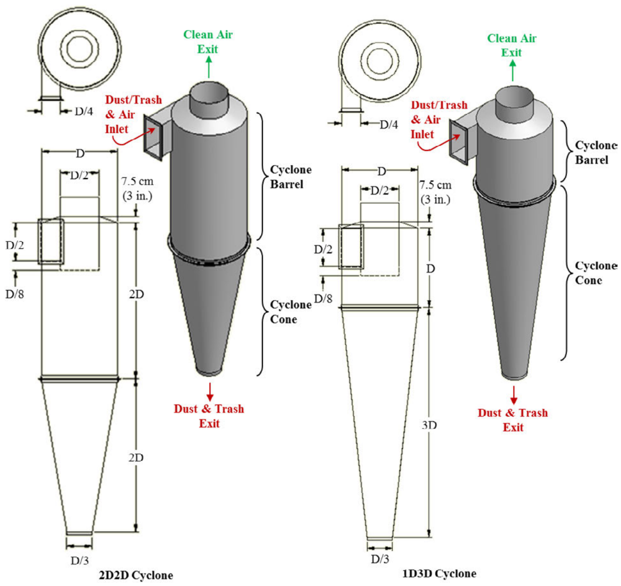

Figure 5. 2D2D and 1D3D cyclone schematics.

METHODS

Two advisory groups were established for this project. The industry group consisted of cotton ginning industry leaders and university and government researchers. The air quality group included members from state and federal regulatory agencies and university and government researchers. These groups were formed to aid in project planning, gin selection, data analysis, and reporting. The project plan was described in detail by Buser et al. (2012).

Seven cotton gins were sampled across the cotton belt. Key factors for selecting specific cotton gins included: 1) facility location, 2) production capacity, 3) processing systems and 4) abatement technologies. Operating permits, site plans, and aerial photographs were reviewed to evaluate potential sites. On-site visits were conducted on all candidate gins to evaluate the process systems and gather information including system condition, layout, capacities, and standard operation. Using this information, several gins from each selected geographical region were selected and prioritized based on industry advisory group discussions. Final gin selection from the prioritized list was influenced by crop limitations and adverse weather events in the region.

Based on air quality advisory group consensus, EPA Method 201A was used to sample the 3rd stage seed-cotton cleaning system at each gin. Method 201A was revised in 2010 to incorporate options for $PM_{2.5}$ (particulate matter with particle diameter less than or equal to a nominal 2.5-µm aerodynamic equivalent diameter) sampling (CFR, 2010); these revisions did not affect the PM_{10} stack sampling methodology used in this project. Method 201A is a constant sampling rate procedure. For the PM_{10} sampling methodology, the particulate-laden stack gas was withdrawn isokinetically (the velocity of the gas entering the sampler was equal to the velocity of the gas in the stack) through a PM_{10} sizing cyclone and then collected on an in-stack filter (Fig. 6). The methods for retrieving the filter and conducting acetone washes of the sizing cyclone are described in detail in Method 201A (CFR, 2010). The mass of each size fraction was determined by gravimetric analysis and included: > 10 µm (PM_{10} sizing cyclone catch acetone wash) and ≤ 10 µm (PM_{10} sizing cyclone exit acetone wash and filter). The PM_{10} mass was determined by adding the mass of particulates captured on the filter and the ≤ 10 µm wash. Total particulate was determined by adding the PM_{10} mass and the mass of the > 10 µm wash.

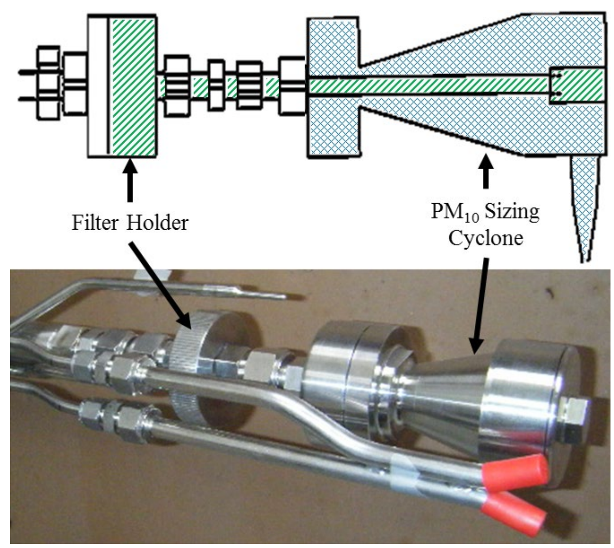

Figure 6. EPA Method 201A PM_{10} sizing cyclone and in-stack filter holder schematic (CFR, 2010) and photograph (▨ ≤ 10 µm, ▩ > 10 µm).

Figure 7 shows the performance curves for the Method 201A sizing cyclones. To measure PM_{10}, the method requires selecting a gas sampling nozzle to achieve a sampling rate that produces a cut size between 9.0 and 11.0 µm at the stack gas temperature. For this study, Method 201A was specifically used to collect filterable PM_{10} emissions (solid particles emitted by a source at the stack and captured in the ≤ 10 µm wash and on the filter [CFR, 2010]).

Only one stack from each 3rd stage seed-cotton cleaning system was tested. For systems with multiple stacks, it was assumed that emissions from each stack of the system were equivalent and the total emissions were calculated by multiplying the measured emission rates by the total number of cyclones used to control the process tested (EPA, 1996a). To obtain reliable results, the same technician from the same certified stack sampling company (Reliable Emissions Measurements, Auberry, CA), trained and experienced in stack sampling cotton gins, conducted the tests at all seven cotton gins.

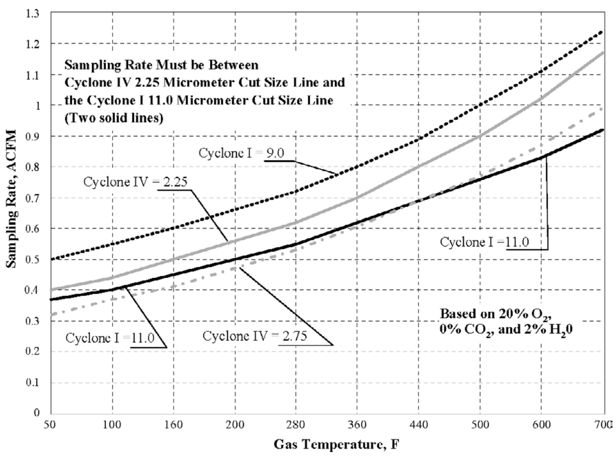

Figure 7. Acceptable sampling rate for sizing cyclones (CFR, 2010) Cyclone I = PM_{10} sizing cyclone (Gas temperatures for the 3rd stage seed-cotton cleaning systems ranged from 25 to 50°C [77-122°F]).

All stack sampling equipment, including the sizing cyclone, was purchased from Apex Instruments (Fuquay-Varina, NC) and met specifications of Method 201A. The sampling media were 47 µm Zefluor filters (Pall Corporation, Port Washington, NY) and the sample recovery and analytical reagent was American Chemical Society certified acetone (A18-4, Fisher Chemical, Pittsburgh, PA – assay ≥ 99.5%). Filters and wash tubs and lids were prelabeled, pre-weighed, and stored in sealed containers at the USDA-ARS Air Quality Lab (AQL) in Lubbock, TX, and then transported to each test site. Prior to testing, the certified stack testing technician calibrated and checked all sampling equipment according to EPA Method 201A.

Each cyclone selected for testing was fitted with a cyclone stack extension that incorporated two sampling ports (90° apart) and airflow straightening vanes to eliminate the cyclonic flow of the air exiting the cyclone (Fig. 8). The extensions were designed to meet EPA criteria (EPA, 1989) with an overall length of 3 m (10 ft) and sampling ports 1.2-m (48-in) downstream from the straightening vanes and 0.9-m (36-in.) upstream from the extension exit.

Figure 8. Schematic and photographs of stack extensions with sampling ports and staightening vanes (rail attached to extension above sampling port, at right, supports sampling probe during testing traverse).

The tests were conducted by the certified stack sampling technician in an enclosed sampling trailer at the base of the cyclone bank (Fig. 9). Sample retrieval, including filters and sampler head acetone washes, was conducted according to Method 201A. After retrieval, filters were sealed in individual Petri dishes and acetone washes were dried on-site in a conduction oven at 49°C (120°F) and then sealed with pre-weighed lids and placed in individual plastic bags for transport to the AQL in Lubbock, TX for gravimetric analyses. During testing, bale data (ID number, weight, and date/time of bale pressing) were either manually recorded by the bale press operator or captured electronically by the gin's computer system for use in calculating emission factors in terms of kg/227-kg bale (lb/500-lb bale). Emission factors and rates were calculated in accordance with Method 201A and ASAE Standard S582 (ASABE, 2005).

All laboratory analyses were conducted at the AQL. All filters were conditioned in an environmental chamber (21 ± 2°C [70 ± 3.6°F]; 35 ± 5% RH) for 48 h prior to gravimetric analyses. Filters were weighed in the environmental chamber on a Mettler MX-5 microbalance (Mettler-Toledo Inc., Columbus, OH – 1 µg readability and 0.9 µg repeatability) after being passed through an anti-static device. The MX-5 microbalance was leveled on a marble table and housed inside an acrylic box to minimize the effects of air currents and vibrations. To reduce recording errors, weights were electronically transferred from the microbalance directly to a spreadsheet. Technicians wore latex gloves and a particulate respirator mask to avoid contamination. AQL procedures required that each sample be weighed three times. If the standard deviation of the weights for a given sample exceeded 10 µg, the sample was reweighed. Gravimetric procedures for the acetone wash tubs were the same as those used for filters.

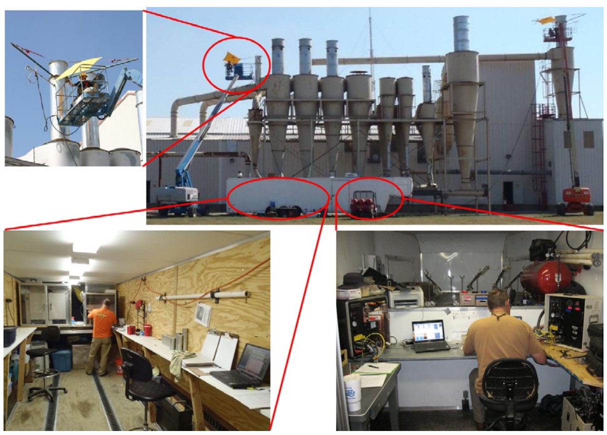

Figure 9. Clockwise from top right: cotton gin stack sampling with air quality lab trailer and technicians on lifts; certified stack sampling technician in the trailer control room conducting tests; sample recovery in trailer clean room; technician operating the probe at stack level.

In addition to gravimetric analyses, each sample was visually inspected for unusual characteristics, such as cotton lint content or extraneous material. Digital pictures were taken of all filters and washes for documentation purposes prior to further analyses. After the laboratory analyses were completed all stack sampling, cotton gin production, and laboratory data were merged.

Two of the seven gins were equipped with 3rd stage seed-cotton cleaning systems. Both 3rd stage seed-cotton cleaning systems sampled at gins A and C were typical for the industry. The 3rd stage seed-cotton cleaning systems at gin A utilized two, separate and parallel, systems (Fig. 10). In each of these parallel systems, the seed-cotton material was pneumatically conveyed from the 2nd stage seed-cotton cleaning system with heated air through a dryer to a seed-cotton cleaner. The material was separated from the airstream by the cleaner. The air from each of the parallel 3rd stage seed-cotton cleaning systems then passed through separate fans and exhausted through separate cyclones. Gin C also utilized two, parallel 3rd stage seed-cotton cleaning systems with single cleaners, except there were no dryers before the cleaners (Fig. 11).

Both 3rd stage seed-cotton cleaning systems sampled utilized 1D3D cyclones to control emissions (Fig. 5), but there were some cyclone design variations among the gins (Table 1 and Fig. 12). Gin C split the system exhaust flow between two cyclones in a dual configuration (side-by-side as opposed to one-behind-another). The system airstream for gin A was exhausted through a single cyclone. Inlets on the gin A and C 3rd stage seed-cotton cleaning cyclones were inverted 1D3D and 2D2D inlets, respectively. Expansion chambers were present on 3rd stage seed-cotton cleaning cyclones at both gins. All of the cyclone configurations outlined above, if properly designed and maintained, are recommended for controlling cotton gin emissions (Whitelock et al., 2009).

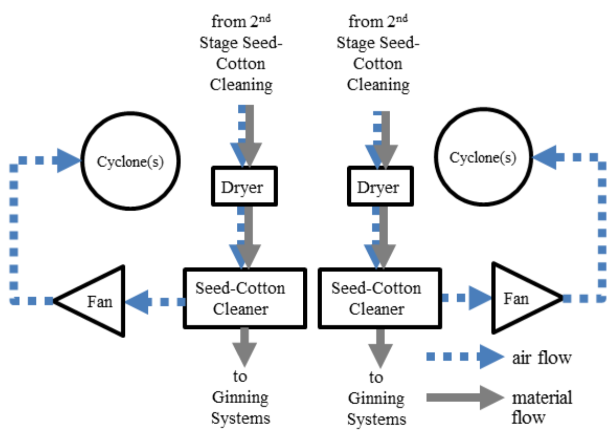

Figure 10. Schematic of split stream, single cleaner 3rd stage seed-cotton cleaning system with dryer (gin A).

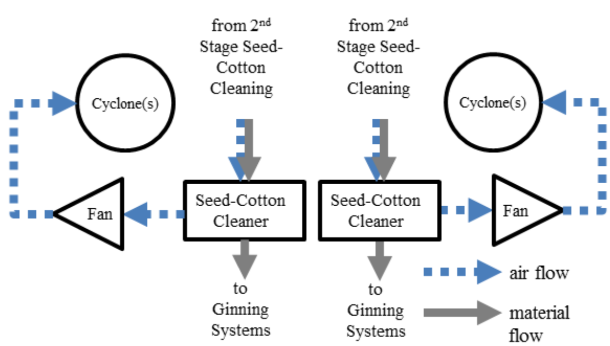

Figure 11. Schematic of split stream, single cleaner 3rd stage seed-cotton cleaning system without dryer (gin C).

Table 1. Abatement device configuration[z] for 3rd stage seed-cotton cleaning systems tested.

Gin	Cyclone Type	Inlet Design[y]	Systems per Gin	Cyclones per Gin	Configuration	Cone Design	Trash Exits to[x]
A	1D3D	inverted 1D3D	2	2	single	expansion chamber	hopper
C	1D3D	2D2D	2	4	dual	expansion chamber	hopper

[z] Figures 5 and 12

[y] Inverted 1D3D inlet has duct in line with the bottom of the inlet

[x] Systems to remove material from cyclone trash exits: hopper = large storage container directly under cyclone trash exit

Figure 12. Cyclone design variations for the tested systems (left to right): dual configuration that splits flow between identical 1D3D cyclones with 2D2D inlets; 1D3D cyclone with an inverted 1D3D inlet; and 1D3D cyclone with 2D2D inlet and expansion chamber on the cone.

RESULTS

Table 2 shows the test parameters for each Method 201A test run for the 3rd stage seed-cotton cleaning systems sampled at the two gins. The system average ginning rate was 22.0 bales/h and the test average ginning rates at each gin ranged from 21.5 to 22.6 bales/h (based on 227-kg [500-lb] equivalent bales). The capacity of gins sampled was representative of the industry average, approximately 25 bales/h. The 1D3D cyclones at gin C were operated with inlet velocities within design criteria, 16.3 ± 2 m/s (3200 ± 400 fpm), but the cyclones at gin A were outside the design range due to limitations in available system adjustments.

There are criteria specified in EPA Method 201A for test runs to be valid for PM_{10} or total particulate measurements (CFR, 2010). Isokinetic sampling and PM_{10} aerodynamic cut size must fall within EPA defined ranges (100 ± 20% and 10.0 ± 1.0 µm, respectively) for valid PM_{10} test runs. All tests met both criteria (Table 2). To use the method to also obtain total filterable particulate, sampling must be within 90 to 110% of isokinetic flow. This criterion was not met in the first test run for gin C; thus the data associated with this run were omitted from the total particulate test averages. Sampling rates ranged from 12.3 to 13.5 standard l/min (0.435-0.476 standard ft^3/min). The stack gas temperatures ranged from 25 to 50°C (77-122°F).

Table 2. Cotton gin production data and stack sampling performance metrics for the 3rd stage seed-cotton cleaning systems.

Gin	Test Run	Ginning Rate, bales/h[z]	Cyclone Inlet Velocity,		Isokinetic Sampling, %	Aerodynamic Cut Size D_{50}, PM_{10} µm	Sampling Rate[y]		Stack Temperature	
			m/s	fpm			slpm	scfm	°C	°F
A	1	21.5	19.4	3824	103	10.0	13.2	0.466	25	77
	2	23.1	18.9	3721	97	9.9	13.5	0.476	28	83
	3	23.0	18.9	3725	96	10.0	13.4	0.474	32	89
Test Average		22.6	19.1	3757						
C	1	21.8	17.3	3397	80[x]	10.8	12.3	0.435	50	122
	2	22.7	17.4	3428	97	10.7	12.5	0.441	49	120
	3	19.9	17.5	3442	99	10.5	12.7	0.448	47	117
Test Average		21.5	17.4	3423						
System Average		22.0	18.2	3590						

[z] 227 kg (500 lb) equivalent bales

[y] slpm = standard l/min, scfm = standard ft^3/min

[x] Did not meet total particulate isokinetic sampling rate criteria (100 ± 10%)

PM_{10} emissions data (ginning and emission rates and corresponding emission factors) for the 3rd stage seed-cotton cleaning systems are shown in Table 3. The system average PM_{10} emission factor was 0.019 kg/bale (0.042 lb/bale). The test average emission factors ranged from 0.012 to 0.026 kg (0.027-0.058 lb) per bale and emission rates ranged from 0.28 to 0.56 kg/h (0.61-1.24 lb/h). Total particulate emissions data (ginning and emission rates and corresponding emission factors) for the 3rd stage seed-cotton cleaning systems are shown in Table 4. The system average total particulate emission factor was 0.024 kg/bale (0.054 lb/bale). The test average emission factors ranged from 0.016 to 0.033 kg (0.035-0.072 lb) per bale. The test average total particulate emission rates ranged from 0.36 to 0.70 kg/h (0.80-1.54 lb/h). The ratio of PM_{10} to total particulate was 79.1% (ratios calculated using tables 3 and 4 may vary slightly from those listed due to rounding).

Table 3. PM_{10} emissions data for the 3rd stage seed-cotton cleaning systems.

Gin	Test Run	Emission Rate,		Emission Factor,	
		kg/h	lb/h	kg/bale^z	lb/bale^z
A	1	0.28	0.62	0.013	0.029
	2	0.32	0.71	0.014	0.031
	3	0.22	0.49	0.010	0.021
Test Average (n=3)		0.28	0.61	0.012	0.027
C	1	0.62	1.36	0.028	0.062
	2	0.57	1.27	0.025	0.056
	3	0.50	1.10	0.025	0.055
Test Average (n=3)		0.56	1.24	0.026	0.058
System Average (n=2)				0.019	0.042

z 227 kg (500 lb) equivalent bales

Table 4. Total particulate emissions data for the 3rd stage seed-cotton cleaning systems.

Gin	Test Run	Emission Rate,		Emission Factor,	
		kg/h	lb/h	kg/bale^z	lb/bale^z
A	1	0.40	0.89	0.019	0.041
	2	0.38	0.85	0.017	0.037
	3	0.30	0.66	0.013	0.028
Test Average (n=3)		0.36	0.80	0.016	0.035
C	1^y	0.78	1.72	0.036	0.079
	2	0.78	1.71	0.034	0.075
	3	0.62	1.36	0.031	0.068
Test Average (n=2)		0.70	1.54	0.033	0.072
System Average (n=2)				0.024	0.054

z 227 kg (500 lb) equivalent bales

y Test run omitted from test averages because isokinetic sampling rate (100 ± 10%) was not met

The average 3rd stage seed-cotton cleaning system total particulate emission factor for this project was about 57% of the EPA AP-42 published value for the No. 3 dryer and cleaner (EPA, 1996a, 1996b), which is an equivalent system to the 3rd stage seed-cotton cleaning system. The range of test average total particulate emission factors determined for this project was lower than the range of AP-42 emission factor data. The average 3rd stage seed-cotton cleaning system PM_{10} emission factor for this project was 1.29 times the EPA AP-42 published value for the No. 3 dryer and cleaner. The test average PM_{10} emission factor range encompassed the AP-42 emission factor data range.

Figure 13 shows an example of samples recovered from a typical 3rd stage seed-cotton cleaning system test run. Often, there were cotton lint fibers, which have cross-sectional diameters much greater than 10 µm, in the cotton gin cyclone exhausts. Therefore, it was not unusual to find lint fiber in the > 10 µm wash from Method 201A. However, lint fibers could pass through the PM_{10} cyclone and collect in the ≤ 10 µm wash and on the filter. This type of material carryover can bias the gravimetric measurements and affect reported PM_{10} emission data. EPA Method 201A does not suggest methods to account for these anomalies. Thus, no effort was made to adjust the data reported in this manuscript to account for these issues.

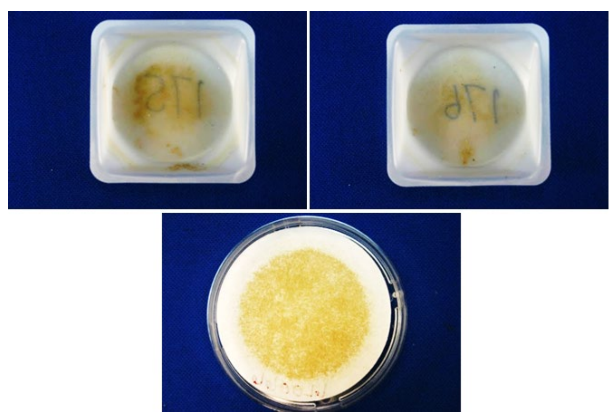

Figure 13. Typical EPA Method 201A filter and sampler head acetone washes from the 3rd stage seed-cotton cleaning system. Clockwise from top left: > 10 µm wash, ≤ 10 µm wash, and filter.

SUMMARY

Seven cotton gins across the U.S. cotton belt were sampled using EPA Method 201A to collect additional data to improve the EPA AP-42 PM_{10} emission factor quality ratings for cotton gins. Two of the seven gins were equipped with 3rd stage seed-cotton cleaning systems. The tested systems were similar in design and typical of the ginning industry. Both systems were equipped with 1D3D cyclones for emissions control with some slight variations in inlet and cone design. In terms of capacity, the two gins were typical of the industry, averaging 22.0 bales/h during testing. The 3rd stage seed-cotton cleaning system average emission factors for PM_{10} and total particulate were 0.019 kg/227-kg bale (0.042 lb/500-lb bale) and 0.024 kg/bale (0.054 lb/bale), respectively. The system average PM_{10} emission factor was higher and the system average total particulate emission factor was lower than those currently published in EPA AP-42. Gin test average PM_{10} and total particulate emission rates ranged from 0.28 to 0.56 kg/h (0.61-1.24 lb/h) and 0.36 to 0.70 kg/h (0.80-1.54 lb/h), respectively. Based on the 3rd stage seed-cotton cleaning system project emission factors, the ratio of PM_{10} to total particulate was 79.1%.

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