The *Journal of Cotton Science 17:447–456 (2013)*
http://journal.cotton.org, © The Cotton Foundation 2013

ENGINEERING AND GINNING

Combined Mote System $PM_{2.5}$ Emission Factors and Rates for Cotton Gins: Method 201A Combination PM_{10} and $PM_{2.5}$ Sizing Cyclones

J. Clif Boykin, Michael D. Buser*, Derek P. Whitelock, and Gregory A. Holt

ABSTRACT

This report is part of a project to characterize cotton gin emissions from the standpoint of stack sampling. In 2006, the Environmental Protection Agency (EPA) finalized and published a more stringent standard for particulate matter with nominal diameter less than or equal to 2.5 µm ($PM_{2.5}$). This created an urgent need to collect additional cotton gin emissions data to address current regulatory issues, because current EPA AP-42 cotton gin $PM_{2.5}$ emission factors did not exist. The objective of this study was the development of $PM_{2.5}$ emission factors for cotton gin combined mote systems based on the EPA-approved stack sampling methodology, Method 201A. The project plan included sampling seven cotton gins across the Cotton Belt. Two of the seven gins had first and second-stage mote systems where the exhaust airstreams were combined. In terms of capacity, the two gins were typical of the industry, averaging 35.1 bales/h during testing. Some test runs were excluded from the test averages because they failed to meet EPA Method 201A Test criteria. Also, other test runs, included in the analyses, had cotton lint fibers that collected in the ≤ 10 µm and/or ≤ 2.5 µm samples. This larger lint material can impact the reported emissions data, but EPA Method 201A does not suggest methods to account for these anomalies. Average measured combined mote system $PM_{2.5}$ emission factor based on the two tests (six total test runs) was 0.0095 kg/227-kg bale (0.021 lb/500-lb bale). The combined mote system emission factors for PM_{10} and total particulate were 0.137 kg/bale (0.301 lb/bale) and 0.141 kg/bale (0.311 lb/bale), respectively. The combined mote system $PM_{2.5}$ emission rate from test averages ranged from 0.21 to 0.45 kg/h (0.47-0.99 lb/h). System average PM_{10} and total particulate emission factors were higher than those currently published in EPA AP-42. The ratios of combined mote system $PM_{2.5}$ to total particulate, $PM_{2.5}$ to PM_{10}, and PM_{10} to total particulate were 6.7, 7.0, and 96.7%, respectively.

In 2006, the United States (U.S.) Environmental Protection Agency (EPA) finalized a more stringent standard for particulate matter with a particle diameter less than or equal to a nominal 2.5-mm ($PM_{2.5}$) aerodynamic equivalent diameter (CFR, 2006). The cotton industry's primary concern with this standard was that published cotton gin $PM_{2.5}$ emissions data did not exist. Cotton ginners' associations across the Cotton Belt, including the National, Texas, Southern, Southeastern, and California associations, have agreed that there is an urgent need to collect $PM_{2.5}$ cotton gin emissions data to address the implementation of the $PM_{2.5}$ standards. Working with cotton ginning associations across the country and state and federal regulatory agencies, Oklahoma State University and USDA-Agricultural Research Service (ARS) researchers developed a proposal and sampling plan that was initiated in 2008 to address this need for additional data. This report is part of a series that details cotton gin emissions measured by stack sampling. Each manuscript in the series addresses a specific cotton ginning system. The systems covered in the series include: unloading, first-stage seed cotton cleaning, second-stage seed cotton cleaning, third-stage seed cotton cleaning, overflow, first-stage lint cleaning, second-stage lint cleaning, combined lint cleaning, cyclone robber, first- stage mote, second-stage mote, combined mote, mote cyclone robber, mote cleaner, mote trash, battery condenser and master trash. This report focuses on $PM_{2.5}$ emissions from combined mote systems.

J.C. Boykin, USDA-ARS Cotton Ginning Research Unit, Stoneville, MS 38776; M.D. Buser*, Oklahoma State University, Stillwater, OK 74078; D.P. Whitelock, USDA-ARS Southwestern Cotton Ginning Research Laboratory, Mesilla Park, NM 88047; and G.A. Holt, USDA-ARS Cotton Production and Processing Research Unit, Lubbock, TX 79401
*Corresponding author: buser@okstate.edu

There are published PM_{10} (particulate matter with a particle diameter less than or equal to a nominal 10-mm aerodynamic equivalent diameter) and total particulate emission factors for cotton gins in EPA's *Compilation of Air Pollution Emission Factors*, AP-42 (EPA, 1996a, 1996b); however, there are no $PM_{2.5}$ emission factors. The AP-42 average PM_{10} emission factor for the mote fan, which is an equivalent system to the combined first and second-stage mote systems was 0.060 kg (0.13 lb) per 217-kg (480-lb) equivalent bale with a range of 0.023 to 0.14 kg (0.050-0.30 lb) per bale. The AP-42 average total particulate emission factor for the mote fan was 0.13 kg (0.28 lb) per bale with a range of 0.045 to 0.47 kg (0.099-1.0 lb) per bale. These PM_{10} and total factors were based on six and nine tests, respectively, and were assigned EPA emission factor quality ratings of D; the second lowest possible rating (EPA, 1996a).

Seed cotton is a perishable commodity that has no real value until the fiber and seed are separated (Wakelyn et al., 2005). Cotton must be processed or ginned, to separate the fiber and seed, producing 227-kg (500-lb) bales of marketable cotton fiber. Cotton ginning is considered an agricultural process and an extension of the harvest by several federal and state agencies (Wakelyn et al., 2005). Although the main function of the cotton gin is to remove the lint fiber from the seed, many other processes also occur during ginning, such as cleaning, drying, and packaging the lint. Pneumatic conveying systems are the primary method of material handling in the cotton gin. As material reaches a processing point, the conveying air is separated and emitted outside the gin through a pollution control device. The amount of dust emitted by a system varies with the process and the condition of the material in the process.

Cotton ginning is a seasonal industry with the ginning season lasting from 75 to 120 days, depending on the size and condition of the crop. Although the trend for U.S. cotton production remained generally flat at about 17 million bales per year during the last 20 years, production from one year to the next often varies greatly for various reasons, including climate and market pressure (Fig. 1). The number of active gins in the U.S. has not remained constant, but has declined to less than 700 in 2011. Consequently, the average volume of cotton handled by each gin has risen and gin capacity has increased to an average of about 25 bales per hour across the U.S. Cotton Belt (Valco et al., 2003, 2006, 2009, 2012).

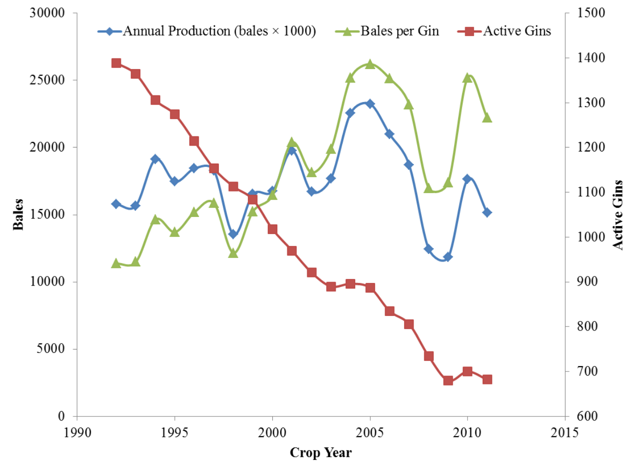

Figure 1. Annual U.S. cotton production, active U.S. gins, and average ginning volume (bales per gin) (NASS, 1993-2012).

Typical cotton gin processing systems include: unloading system, dryers, seed cotton cleaners, gin stands, overflow collector, lint cleaners, battery condenser, bale packaging system, and trash handling systems (Fig. 2); however, the number and type of machines and processes can vary. Each of these systems serves a unique function with the ultimate goal of ginning the cotton to produce a marketable product. Raw seed cotton harvested from the field is compacted into large units called "modules" for delivery to the gin. The unloading system removes seed cotton either mechanically or pneumatically from the module feed system and conveys the seed cotton to the seed cotton cleaning systems. Seed cotton cleaning systems dry the seed cotton and remove foreign matter prior to ginning. Ginning systems also remove foreign matter and separate the cotton fiber from the seed. Lint cleaning systems further clean the cotton lint after ginning. The battery condenser and packaging systems combine lint from the lint cleaning systems and compress the lint into dense bales for easy transport. Gin systems produce some type of by-product or trash, such as rocks, soil, sticks, hulls, leaf material, and short or tangled immature fiber (motes), as a result of processing the seed cotton or lint. These streams of by-products must be removed from the machinery and handled by trash collection systems. These trash systems typically further process the by-products (e.g., mote cleaners) and/or consolidate the trash from the gin systems into a hopper or pile for subsequent removal.

After the seed and lint are separated at the gin stand, the lint is cleaned by one or more stages of lint cleaners. The material removed by lint cleaners is referred to as “motes” and is handled by the mote systems (Fig. 3). Motes are pneumatically conveyed by suction away from the lint cleaners, through a centrifugal fan, to one or two particulate abatement cyclones. Depending on the gin facility, the first and second stages of lint cleaning may be combined and share a mote system, thus sharing a fan and abatement devices, or lint cleaning stages may have mote systems that operate independently with separate fans and cyclones. The function of the first and second-stage mote systems with separate or combined exhausts is the same and it is expected that the PM emissions from a combined mote system would be similar to summation of the first and second-stage mote systems with separate exhausts. The material handled by the mote cyclones typically includes small trash and particulate, and large amounts of lint fibers (Fig. 4).

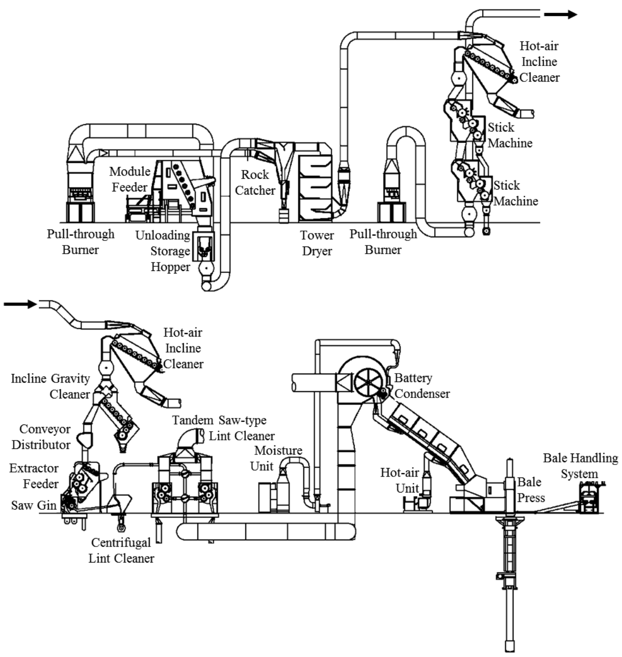

Figure 2. Typical modern cotton gin layout (Courtesy Lummus Corporation, Savannah, GA).

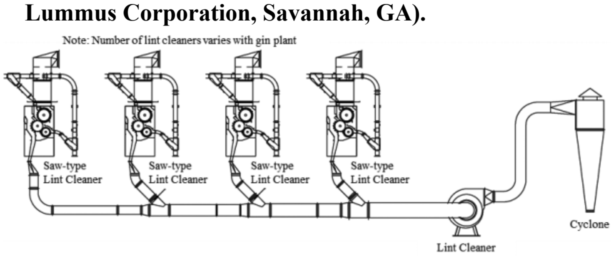

Figure 3. Typical cotton gin combined mote system layout (Courtesy Lummus Corporation, Savannah, GA).

Figure 4. Photograph of typical trash captured by the combined mote system cyclones.

Cyclones are the most common particulate matter abatement devices used at cotton gins. Standard cyclone designs used at cotton ginning facilities are the 2D2D and 1D3D (Whitelock et al., 2009). The first D in the designation indicates the length of the cyclone barrel relative to the cyclone barrel diameter, and the second D indicates the length of the cyclone cone relative to the cyclone barrel diameter. A standard 2D2D cyclone (Fig. 5) has an inlet height of D/2 and width of D/4 and design inlet velocity of 15.2 ± 2 m/s (3000 ± 400 fpm). The standard 1D3D cyclone (Fig. 5) has the same inlet dimensions as the 2D2D or may have the original 1D3D inlet with height of D and width D/8. Also, it has a design inlet velocity of 16.3 ± 2 m/s (3200 ± 400 fpm).

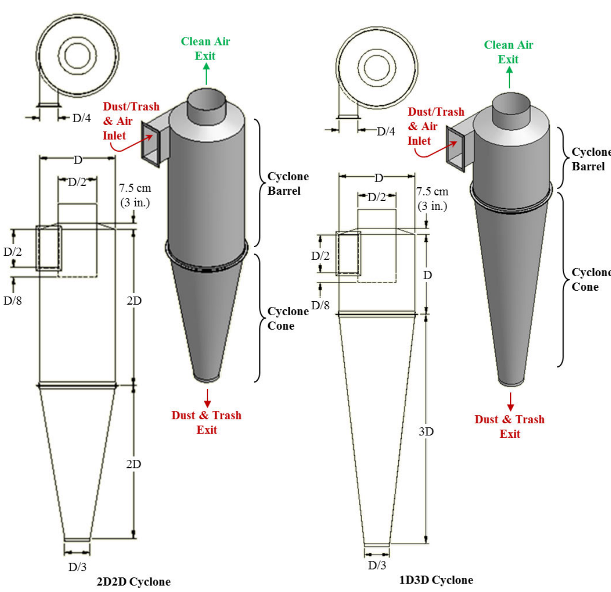

Figure 5. 2D2D and 1D3D cyclone schematics.

The objective of this study was the development of $PM_{2.5}$ emission factors for cotton gin combined mote systems with cyclones for emissions control based on EPA-approved stack sampling methodologies.

METHODS

Two advisory groups were established for this project. The industry group consisted of cotton ginning industry leaders and university and government researchers. The air quality group included members from state and federal regulatory agencies and university and government researchers. Both groups were formed to aid in project planning, gin selection, data analyses, and reporting. The project plan is described in detail by Buser et al. (2012).

Seven cotton gins were sampled across the Cotton Belt. Key factors for selecting specific cotton gins included: 1) facility location (geographically diverse), 2) industry representative production capacity, 3) typical processing systems and 4) gins equipped with properly designed and maintained 1D3D cyclones. Operating permits, site plans, and aerial photographs were reviewed to evaluate potential sites. On-site visits were conducted on all candidate gins to evaluate the process systems and gather information including system condition, layout, capacities, and standard operation. Using this information, several gins from each selected geographical region were selected and prioritized based on industry advisory group discussions. Final gin selection from the prioritized list was influenced by crop limitations and adverse weather events in the region.

Based on air quality advisory group consensus, EPA Other Test Method 27 (OTM27) was used to sample the combined mote system at each gin. When testing for this project began in 2008, OTM27 was the EPA method for determination of PM_{10} and $PM_{2.5}$ from stationary sources. In December 2010, OTM27 was replaced with a revised and finalized Method 201A (CFR, 2010). The revised Method 201A was a successor of OTM27. The two methods were similar to the point that EPA stated in an answer to a frequently asked question for Method 201A (EPA, 2010) that "If the source was using OTM 27 (and 28) for measuring either PM_{10} or $PM_{2.5}$ then using the revised reference methods Method 201A (and 202) should not be a concern and should give equivalent results." Accordingly, OTM27 is no longer an EPA method that can be cited, and the revised Method 201A will be cited in this manuscript. Using Method 201A (CFR, 2010) to sample $PM_{2.5}$, the particulate-laden stack gas was withdrawn isokinetically (the velocity of the gas entering the sampler was equal to the velocity of the gas in the stack) through a PM_{10} sizing cyclone and a $PM_{2.5}$ sizing cyclone, and then collected on an in-stack filter (Fig. 6). The methods for retrieving the filter and conducting acetone washes of the sizing cyclones are described in detail in Method 201A (CFR, 2010). The mass of each size fraction was determined by gravimetric analysis and included: > 10 µm (PM_{10} sizing cyclone catch acetone wash); 10 to 2.5 µm (PM_{10} sizing cyclone exit acetone wash and $PM_{2.5}$ sizing cyclone catch acetone wash); and ≤ 2.5 µm ($PM_{2.5}$ sizing cyclone exit acetone wash and filter). The $PM_{2.5}$ mass was determined by adding the mass of particulates captured on the filter and the ≤ 2.5 µm wash. The PM_{10} mass was determined by adding the $PM_{2.5}$ mass and the mass of the 10 to 2.5 µm wash. Total particulate was determined by adding the PM_{10} mass and the mass of the > 10 µm wash.

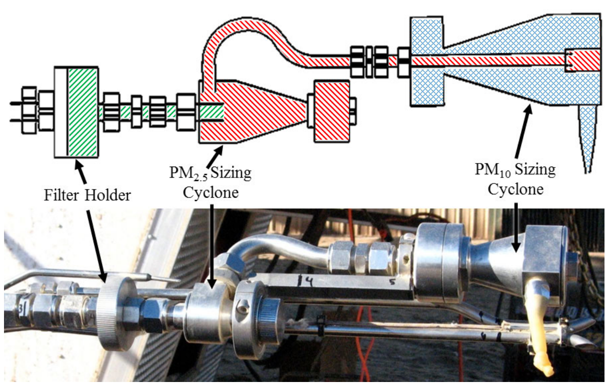

Figure 6. EPA Method 201A PM_{10} and $PM_{2.5}$ sizing cyclones and in-stack filter holder schematic (CFR, 2010) and photograph (≤ 2.5 µm, 10 to 2.5 µm, > 10 µm).

Figure 7 shows the performance curves for the PM_{10} and $PM_{2.5}$ sizing cyclones. To measure both PM_{10} and $PM_{2.5}$, Method 201A requires selecting a gas sampling rate in the middle of the overlap zone of the performance curves for both sizing cyclones. For this study, the method was specifically used to collect filterable $PM_{2.5}$ emissions (solid particles emitted by a source at the stack and captured in the ≤ 2.5 µm wash and on the filter [CFR, 2010]). The PM_{10} sizing cyclone was used to scrub larger particles from the airstream to minimize their impact on the $PM_{2.5}$ sizing cyclone. Thus, the gas sampling rate was targeted to optimize the $PM_{2.5}$ cyclone performance.

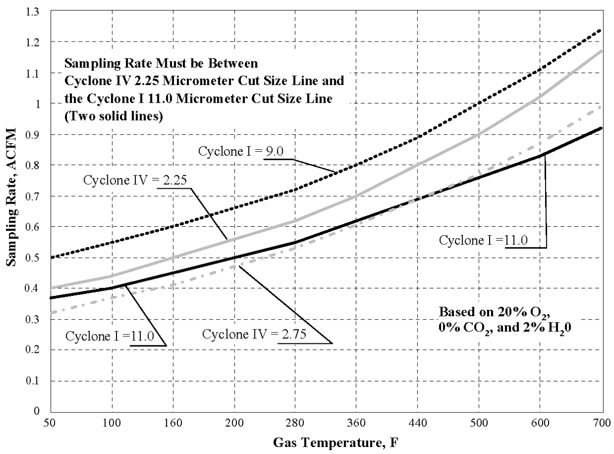

Figure 7. Acceptable sampling rate for combined cyclone heads (CFR, 2010). Cyclone I = PM_{10} sizing cyclone and Cyclone IV = $PM_{2.5}$ sizing cyclone (Gas temperatures for the combined mote systems tested ranged from 22 to 33°C [71-92°F]).

Only one stack from each combined mote system was tested. For systems with multiple stacks, it was assumed that emissions from each stack of the system were equivalent and the total emissions were calculated by multiplying the measured emission rates by the total number of cyclones used to control the process tested (EPA, 1996a). To obtain reliable results, the same technician from the same certified stack sampling company (Reliable Emissions Measurements, Auberry, CA), trained and experienced in stack sampling cotton gins, conducted the tests at all seven cotton gins.

All stack sampling equipment, including the sizing cyclones, was purchased from Apex Instruments (Fuquay-Varina, NC) and met specifications of Method 201A. The sampling media were 47 mm Zefluor filters (Pall Corporation, Port Washington, NY) and the sample recovery and analytical reagent was American Chemical Society certified acetone (A18-4, Fisher Chemical, Pittsburgh, PA – assay ≥ 99.5%)). Filters and wash tubs and lids were prelabeled and pre-weighed and stored in sealed containers at the USDA-ARS Air Quality Lab (AQL) in Lubbock, TX, and then transported to each test site. Prior to testing, the certified stack testing technician conducted calibrations and checks on all stack sampling equipment according to EPA Method 201A.

Each cyclone tested was fitted with a cyclone stack extension that incorporated two sampling ports (90° apart) and airflow straightening vanes to eliminate the cyclonic flow of the air exiting the cyclone (Fig. 8). The extensions were designed to meet EPA criteria (EPA, 1989) with an overall length of 3 m (10 ft) and sampling ports 1.2-m (48-in) downstream from the straightening vanes and 0.9-m (36-in) upstream from the extension exit.

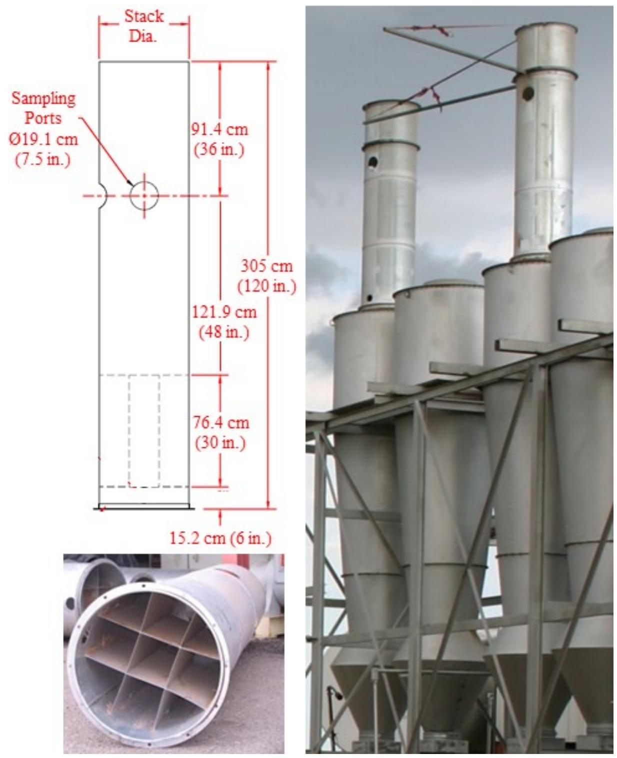

Figure 8. Schematic and photographs of stack extensions with sampling ports and staightening vanes (rail attached to extension above sampling port, at right, supports sampling probe during testing traverse).

The tests were conducted by the certified stack-sampling technician in an enclosed sampling trailer at the base of the cyclone bank (Fig. 9). Sample retrieval, including filters and sampler head acetone washes, was conducted according to Method 201A. After recovery, filters were sealed in individual Petri dishes and acetone washes were dried on-site in a conduction oven at 49°C and then sealed with pre-weighed lids and placed in individual plastic bags for transport to the AQL in Lubbock, TX for gravimetric analyses. During testing, bale data (ID number, weight, and date/time of bale pressing) were either manually recorded by the bale press operator or captured electronically by the gin's computer system for use in calculating emission factors in terms of kg/227-kg bale (lb/500-lb bale). Emission factors and rates were calculated in accordance with Method 201A and American Society of Agricultural and Biological Engineers (ASAE) Standard S582 (ASABE, 2005).

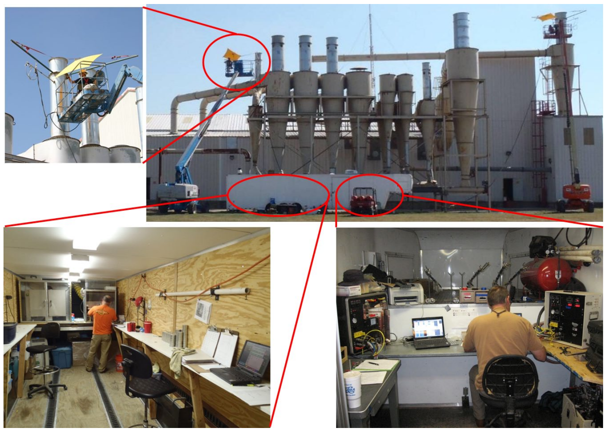

Figure 9. Clockwise from top right: cotton gin stack sampling with air quality lab trailer and technicians on lifts; certified stack sampling technician in the trailer control room conducting tests; sample recovery in trailer clean room; technician operating the probe at stack level.

All laboratory analyses were conducted at the AQL. All filters were conditioned in an environmental chamber (21 ± 2°C; 35 ± 5% RH) for 48 h prior to gravimetric analyses. Filters were weighed in the environmental chamber on a Mettler MX-5 microbalance (Mettler-Toledo Inc., Columbus, OH – 1 µg readability and 0.9 µg repeatability) after being passed through an anti-static device. The MX-5 microbalance was leveled on a marble table and housed inside an acrylic box to minimize the effects of air currents and vibrations. To reduce recording errors, weights were digitally transferred from the microbalance directly to a spreadsheet. Technicians wore latex gloves and a particulate respirator mask to avoid contamination. AQL procedures required that each sample be weighed three times. If the standard deviation of the weights for a given sample exceeded 10 µg, the sample was reweighed. Gravimetric procedures for the acetone wash tubs were the same as those used for filters.

In addition to gravimetric analyses, each sample was visually inspected for unusual characteristics, such as cotton lint content or extraneous material. Digital pictures were taken of all filters and washes for documentation purposes prior to further analyses. After the laboratory analyses were completed all stack sampling, cotton gin production, and laboratory data were merged.

Two of the seven gins were designed so that the exhaust airstreams from the first and second-stage mote systems were combined. The combined systems sampled were typical for the industry, but varied among the gins. As the lint was cleaned in three first-stage lint cleaning systems and then three second-stage lint cleaning systems at gin E, the trash removed from the lint in the six cleaners was combined in the combined mote system and pneumatically conveyed from the lint cleaners through a fan and exhausted through one or more cyclones (Fig. 10). The combined first and second-stage mote system at gin G was essentially the same, except the combined mote system pulled trash from two first-stage lint cleaning systems and two second-stage lint cleaning systems (Fig. 11).

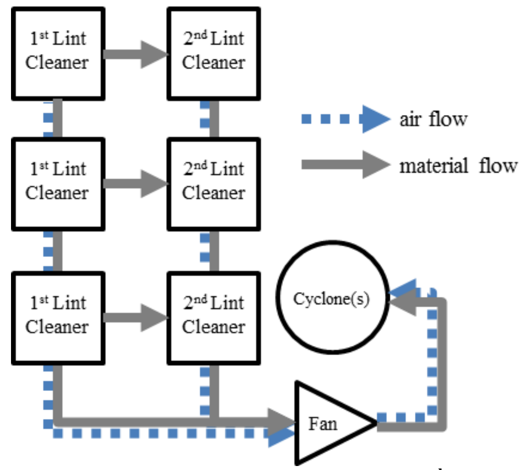

Figure 10. Schematic of combined 1st and 2nd stage mote system pulling material from three 1st and 2nd stage lint cleaning systems (gin E).

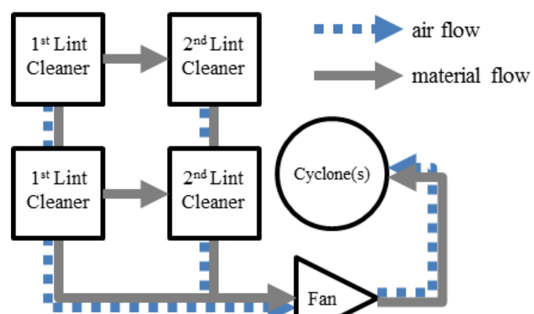

Figure 11. Schematic of combined 1st and 2nd stage mote system pulling material from two 1st and 2nd stage lint cleaning systems (gin G).

All combined mote systems sampled utilized 1D3D cyclones to control emissions (Table 1 and Fig. 5). The system airstream for both gins was exhausted through a single cyclone. Inlets on all the combined mote system cyclones were 2D2D type. Standard cones were present on combined mote system cyclones at all gins. The cyclone tested at gin G had a mote system cyclone robber pulling airflow from its trash exit. This configuration helps remove lint and other trash from the cyclone that could otherwise circulate near the trash exit at the bottom of the cone for a period of time before dropping out. The design characteristics for all of the combined mote system cyclones tested, if properly designed and maintained, are recommended for controlling cotton gin emissions (Whitelock et al., 2009).

Table 1. Abatement device configuration[z] for combined mote systems tested.

Gin	Cyclone Type	Inlet Design	Systems per Gin	Cyclones per Gin	Configuration	Cone Design	Trash exits to[y]
E	1D3D	2D2D	1	1	single	standard	mote cleaner
G	1D3D	2D2D	1	1	single	standard	Robber

[z] Figure 5

[y] Systems to remove material from cyclone trash exits: mote cleaner = gin machine that further cleans fiber captured by system; robber = pneumatic suction system

RESULTS

Table 2 shows the test parameters for each Method 201A test run for the combined mote systems sampled at the two gins. The system average ginning rate was 35.1 bales/h and the test average ginning rates at each gin ranged from 34.2 to 36.0 bales/h (based on 227-kg [500-lb] equivalent bales). The capacity of gins sampled was representative of the industry average, approximately 25 bales/h. The 1D3D cyclones were all operated with inlet velocities within design criteria, 16.3 ± 2 m/s (3200 ± 400 fpm).

There are criteria specified in EPA Method 201A for test runs to be valid for $PM_{2.5}$, PM_{10}, or total particulate measurements (CFR, 2010). Isokinetic sampling must fall within EPA defined ranges (100 ± 20%) for valid $PM_{2.5}$ and PM_{10} test runs. All tests met the isokinetic criteria (Table 2). To use the method to also obtain total filterable particulate, sampling must be within 90 to 110% of isokinetic flow. All test runs were included in the total particulate test averages. The $PM_{2.5}$ aerodynamic cut size must fall within EPA defined ranges (2.50 ± 0.25 mm) for valid $PM_{2.5}$ test runs. $PM_{2.5}$ cut size criteria were met for all test runs. The PM_{10} aerodynamic cut size must fall within EPA defined ranges (10.0 ± 1.0 mm) for valid PM_{10} test runs. PM_{10} cut size criteria were not met in the first and second test runs for gin E, thus the data associated with these runs were omitted from the PM_{10} test averages.

Sampling rates ranged from 10.8 to 11.5 standard l/min (0.382-0.407 standard ft^3/min) (Table 2). The stack gas temperatures ranged from 22 to 33°C. The sampling method documentation (CFR, 2010) warns that the acceptable gas sampling rate range is limited at the stack gas temperatures encountered during this project's testing, as indicated by the narrow difference between the solid lines in Figure 7 for the temperatures listed above. These stack gas characteristics justified targeting the $PM_{2.5}$ cut size criteria and treating the PM_{10} cut size criteria as secondary.

Table 2. Cotton gin production data and stack sampling performance metrics for the combined mote systems.

Gin	Test Run	Ginning Rate, bales/h[z]	Cyclone Inlet Velocity,		Isokinetic Sampling, %	Aerodynamic Cut Size D_{50},		Sampling Rate[y]		Stack Temperature	
			m/s	fpm		$PM_{2.5}$ µm	PM_{10} µm	slpm	scfm	°C	°F
E	1	31.5	17.3	3412	100	2.51	11.3[x]	10.8	0.382	29	85
	2	35.3	16.8	3307	104	2.50	11.3[x]	10.9	0.386	31	88
	3	35.8	17.0	3347	108	2.37	10.9	11.5	0.407	33	92
Test Average		34.2	17.0	3355							
G	1	35.1	16.4	3231	108	2.35	10.9	11.1	0.392	24	75
	2	37.0	16.3	3205	108	2.35	10.9	11.0	0.389	22	72
	3	36.0	16.5	3254	106	2.36	11.0	11.0	0.387	22	71
Test Average		36.0	16.4	3230							
System Average		35.1	16.7	3293							

[z] 227 kg (500 lb) equivalent bales

[y] slpm = standard l/min, scfm = standard ft^3/min

[x] Did not meet PM_{10} (10.0 ± 1.0 µm) aerodynamic cut size criteria

Collected $PM_{2.5}$ emissions data (ginning and emission rates and corresponding emission factors) for the combined mote systems are shown in Table 3. The system average $PM_{2.5}$ emission factor was 0.0095 kg/bale (0.021 lb/bale). The test average emission factors at each gin ranged from 0.0060 to 0.013 kg (0.013-0.029 lb) per bale and $PM_{2.5}$ emission rates ranged from 0.21 to 0.45 kg/h (0.47-0.99 lb/h). PM_{10} emissions data (ginning and emission rates and corresponding emission factors) for the combined mote systems are shown in Table 4. The system average PM_{10} emission factor was 0.137 kg/bale (0.301 lb/bale). The test average emission factors ranged from 0.056 to 0.217 kg (0.124 to 0.478 lb) per bale and emission rates ranged from 2.03 to 7.75 kg/h (4.48-17.10 lb/h). Total particulate emissions data (ginning and emission rates and corresponding emission factors) for the combined mote systems are shown in Table 5. The system average total particulate emission factor was 0.141 kg/bale (0.311 lb/bale). The test average emission factors ranged from 0.081 to 0.202 kg (0.177 to 0.445 lb) per bale. The test average total particulate emission rates ranged from 2.90 to 6.95 kg/h (6.40 to 15.32 lb/h). The ratios of $PM_{2.5}$ to total particulate, $PM_{2.5}$ to PM_{10}, and PM_{10} to total particulate were 6.7, 7.0, and 96.7%, respectively (ratios calculated using tables three, four, and five may vary slightly from those listed due to rounding).

The combined mote system total particulate emission factor average for this project was about 1.11 times the EPA AP-42 published value for the mote fan (EPA, 1996a, 1996b), which is an equivalent system to combined first and second-stage mote systems. The range of test average total particulate emission factors determined for this project fell within the range of AP-42 emission factor data. The combined mote system PM_{10} emission factor average for this project was 2.32 times the EPA AP-42 published value for the mote fan. The test average PM_{10} emission factor range and the AP-42 emission factor data range overlapped.

Figure 12 shows an example of samples recovered from a typical combined mote system test run. Often, there were cotton lint fibers, which have cross-sectional diameters much greater than 2.5 µm, in the cotton gin cyclone exhausts. Therefore, it was not unusual to find lint fiber in the > 10 µm wash from Method 201A. However, in the atypical sample shown in Figure 13, lint fibers passed through the PM_{10} and $PM_{2.5}$ cyclones and were collected on the

Table 3. $PM_{2.5}$ emissions data for the combined mote systems.

Gin	Test Run	Emission Rate,		Emission Factor,	
		kg/h	lb/h	kg/bale[z]	lb/bale[z]
E	1	0.37	0.82	0.012	0.026
	2	0.51	1.11	0.014	0.032
	3	0.46	1.02	0.013	0.029
Test Average (n=3)		0.45	0.99	0.013	0.029
G	1	0.20	0.45	0.0058	0.013
	2	0.25	0.54	0.0066	0.015
	3	0.20	0.43	0.0055	0.012
Test Average (n=3)		0.21	0.47	0.0060	0.013
System Average (n=2)				0.0095	0.021

[z] 227 kg (500 lb) equivalent bales

Table 4. PM_{10} emissions data for the combined mote systems.

Gin	Test Run	Emission Rate,		Emission Factor,	
		kg/h	lb/h	kg/bale[z]	lb/bale[z]
E	1[y]	4.01	8.83	0.127	0.280
	2[y]	4.10	9.03	0.116	0.256
	3	7.75	17.10	0.217	0.478
Test Average (n=1)		7.75	17.10	0.217	0.478
G	1	1.96	4.31	0.056	0.123
	2	2.06	4.54	0.056	0.123
	3	2.08	4.58	0.058	0.127
Test Average (n=3)		2.03	4.48	0.056	0.124
System Average (n=2)				0.137	0.301

[z] 227 kg (500 lb) equivalent bales

[y] Test run omitted from test averages because aerodynamic cut size (10.0 ± 1.0 µm) was not met

Table 5. Total particulate emissions data for the combined mote systems.

Gin	Test Run	Emission Rate,		Emission Factor,	
		kg/h	lb/h	kg/bale[z]	lb/bale[z]
E	1	5.65	12.47	0.179	0.396
	2	5.75	12.68	0.163	0.359
	3	9.44	20.81	0.264	0.582
Test Average (n=3)		6.95	15.32	0.202	0.445
G	1	2.70	5.96	0.077	0.170
	2	2.96	6.52	0.080	0.176
	3	3.04	6.71	0.085	0.187
Test Average (n=3)		2.90	6.40	0.081	0.177
System Average (n=2)				0.141	0.311

[z] 227 kg (500 lb) equivalent bales

filter. This type of material carryover can bias the gravimetric measurements and impact reported $PM_{2.5}$ emission data. EPA Method 201A does not suggest methods to account for these anomalies. Thus, no effort was made to adjust the data reported in this manuscript to account for these issues.

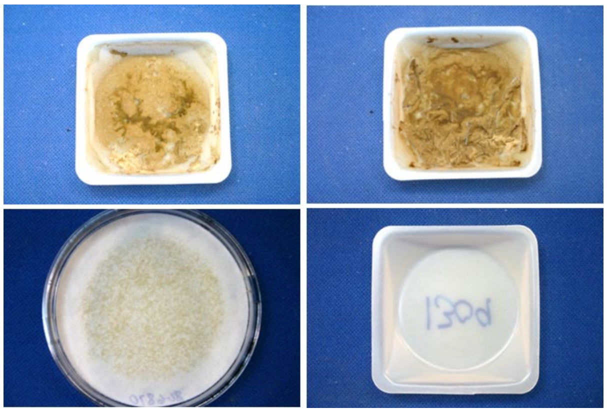

Figure 12. Typical EPA Method 201A filter and sampler head acetone washes from the combined mote system. Clockwise from top left: > 10 µm wash, 10 to 2.5 µm wash, ≤ 2.5 µm wash, and filter.

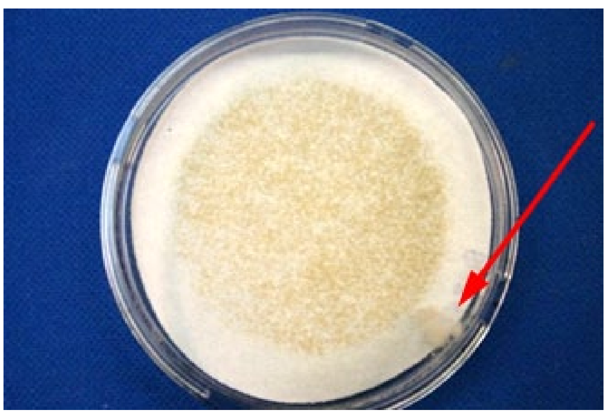

Figure 13. Atypical EPA Method 201A filter from the combined mote system with lint.

SUMMARY

Seven cotton gins across the U.S. Cotton Belt were stack sampled using EPA Method 201A to fill the data gap that exists for $PM_{2.5}$ cotton gin emissions data. Two of the seven gins had first and second-stage mote systems where the exhaust airstreams were combined. All the systems were equipped with 1D3D cyclones for emissions control. In terms of capacity, the two gins were typical of the industry, averaging 35.1 bales/h during testing. Some test runs were excluded from the test averages because they failed to meet EPA Method 201A Test criteria. Also, other test runs, included in the analyses, had cotton lint fibers that collected in the ≤ 10 µm and/or ≤ 2.5 µm samples. This larger lint material can impact the reported emissions data, but EPA Method 201A does not suggest methods to account for these anomalies. Average measured combined mote system $PM_{2.5}$ emission factor based on the two gins tested (six total test runs) was 0.0095 kg/227-kg bale (0.021 lb/500-lb bale). The combined mote system emission factors for PM_{10} and total particulate were 0.137 kg/bale (0.301 lb/bale) and 0.141 kg/bale (0.311 lb/bale), respectively. The gin test average $PM_{2.5}$, PM_{10} and total particulate emission rates ranged from 0.21 to 0.45 kg/h (0.47-0.99 lb/h), 2.03 to 7.75 kg/h (4.48-17.10 lb/h) and 2.90 to 6.95 kg/h (6.40-15.32 lb/h), respectively. System average PM_{10} and total particulate emission factors were higher than those currently published in EPA AP-42. The ratios of combined mote system $PM_{2.5}$ to total particulate, $PM_{2.5}$ to PM_{10}, and PM_{10} to total particulate were 6.7, 7.0, and 96.7%, respectively. These data are the first published data to document $PM_{2.5}$ emissions from combined mote systems at cotton gins.

ACKNOWLEDGEMENT

The authors appreciate the cooperating gin managers and personnel who generously allowed and endured sampling at their gins. In addition, we thank California Cotton Ginners' and Growers' Association, Cotton Incorporated, San Joaquin Valleywide Air Pollution Study Agency, Southeastern Cotton Ginners' Association, Southern Cotton Ginners' Association, Texas Cotton Ginners' Association, Texas State Support Committee, and The Cotton Foundation for funding this project. The authors also thank the Cotton Gin Advisory Group and Air Quality Advisory Group for their involvement and participation in planning, execution, and data analyses for this project that is essential to developing quality data that will be used by industry, regulatory agencies, and the scientific community. The advisory groups included: the funding agencies listed above, California Air Resources Board, Missouri Department of Natural Resources, National Cotton Council, National Cotton Ginners' Association, North Carolina Department of Environment and Natural Resources, San Joaquin Valley Air Pollution Control District, Texas A&M University, Texas Commission on Environmental Quality, USDA-NRCS National Air Quality and Atmospheric Change, and U.S. Environmental Protection Agency (national, Region 4 and 9).

DISCLAIMER

Mention of trade names or commercial products in this publication is solely for the purpose of providing specific information and does not imply recommendation or endorsement by the Oklahoma State University or U.S. Department of Agriculture. Oklahoma State University and USDA are equal opportunity providers and employers.

REFERENCES

American Society of Agricultural and Biological Engineers (ASABE). 2005. Cotton Gins – Method of Utilizing Emission Factors in Determining Emission Parameters. ASAE S582 March 2005. American Society of Agricultural and Biological Engineers, St. Joseph, MI.

Buser, M.D., D.P. Whitelock, J.C. Boykin, and G.A. Holt. 2012. Characterization of cotton gin particulate matter emissions—Project plan. J. Cotton Sci. 16:105–116.

Code of Federal Regulations (CFR). 2006. National ambient air quality standards for particulate matter; final rule. 40 CFR, Part 50. U.S. Government Printing Office, Washington, D.C.

Code of Federal Regulations (CFR). 2010. Method 201A – Determination of PM_{10} and $PM_{2.5}$ emissions from stationary sources (Constant sampling rate procedure). 40 CFR 51 Appendix M. Available at http://www.epa.gov/ttn/emc/promgate/m-201a.pdf (verified 2 Jan. 2013).

Environmental Protection Agency (EPA). 1989. Particulate sampling in cyclonic flow. U.S. Environmental Protection Agency, Washington, DC. Available online at http://www.epa.gov/ttn/emc/guidlnd/gd-008.pdf (verified 2 Jan. 2013).

Environmental Protection Agency (EPA). 1996a. Emission factor documentation for AP-42, Section 9.7, Cotton Ginning, (EPA Contract No. 68-D2-0159; MRI Project No. 4603-01, Apr. 1996).

Environmental Protection Agency (EPA). 1996b. Food and agricultural industries: Cotton gins. *In* Compilation of air pollution emission factors, Volume 1: Stationary point and area sources. Publ. AP-42. U.S. Environmental Protection Agency, Washington, DC.

Environmental Protection Agency (EPA). 2010. Frequently asked questions (FAQS) for Method 201A [Online]. Available at http://www.epa.gov/ttn/emc/methods/method201a.html (verified 01 Jan. 2013).

National Agricultural Statistics Service (NASS).1993-2012. Cotton Ginnings Annual Summary [Online]. USDA National Agricultural Statistics Service, Washington, DC. Available at http://usda.mannlib.cornell.edu/MannUsda/viewDocumentInfo.do?documentID=1042 (verified 2 Jan. 2013).

Valco, T.D., H. Ashley, J.K. Green, D.S. Findley, T.L. Price, J.M. Fannin, and R.A. Isom. 2012. The cost of ginning cotton – 2010 survey results. p. 616–619 *In* Proc. Beltwide Cotton Conference., Orlando, FL 3-6 Jan. 2012. Natl. Cotton Counc. Am., Memphis, TN.

Valco, T.D., B. Collins, D.S. Findley, J.K. Green, L. Todd, R.A. Isom, and M.H. Wilcutt. 2003. The cost of ginning cotton – 2001 survey results. p. 662–670 *In* Proc. Beltwide Cotton Conference., Nashville, TN 6-10 Jan. 2003. Natl. Cotton Counc. Am., Memphis, TN.

Valco, T.D., J.K. Green, R.A. Isom, D.S. Findley, T.L. Price, and H. Ashley. 2009. The cost of ginning cotton – 2007 survey results. p. 540–545 *In* Proc. Beltwide Cotton Conference., San Antonio, TX 5-8 Jan. 2009. Natl. Cotton Counc. Am., Memphis, TN.

Valco, T.D., J.K. Green, T.L. Price, R.A. Isom, and D.S. Findley. 2006. Cost of ginning cotton – 2004 survey results. p. 618–626 *In* Proc. Beltwide Cotton Conference., San Antonio, TX 3-6 Jan. 2006. Natl. Cotton Counc. Am., Memphis, TN.

Wakelyn, P.J., D.W. Thompson, B.M. Norman, C.B. Nevius, and D.S. Findley. 2005. Why Cotton Ginning is Considered Agriculture. *Cotton Gin and Oil Mill Press* 106(8), 5-9.

Whitelock, D.P., C.B. Armijo, M.D. Buser, and S.E. Hughs. 2009 Using cyclones effectively at cotton gins. Appl. Eng. Ag. 25:563–576.